

(19) World Intellectual Property Organization
International Bureau



(43) International Publication Date
12 September 2003 (12.09.2003)

PCT

(10) International Publication Number
WO 03/075432 A2

(51) International Patent Classification⁷: **H02K**
(21) International Application Number: PCT/US03/06065
(22) International Filing Date: 27 February 2003 (27.02.2003)
(25) Filing Language: English
(26) Publication Language: English
(30) Priority Data:
09/683,900 28 February 2002 (28.02.2002) US
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(81) Designated States (*national*): AE, AG, AL, AM, AT, AU, AZ, BA, BB, BG, BR, BY, BZ, CA, CH, CN, CO, CR, CU, CZ, DE, DK, DM, DZ, EC, EE, ES, FI, GB, GD, GE, GH, GM, HR, HU, ID, IL, IN, IS, JP, KE, KG, KP, KR, KZ, LC, LK, LR, LS, LT, LU, LV, MA, MD, MG, MK, MN, MW, MX, MZ, NO, NZ, OM, PH, PL, PT, RO, RU, SD, SE, SG, SK, SL, TJ, TM, TN, TR, TT, TZ, UA, UG, UZ, VN, YU, ZA, ZM, ZW.

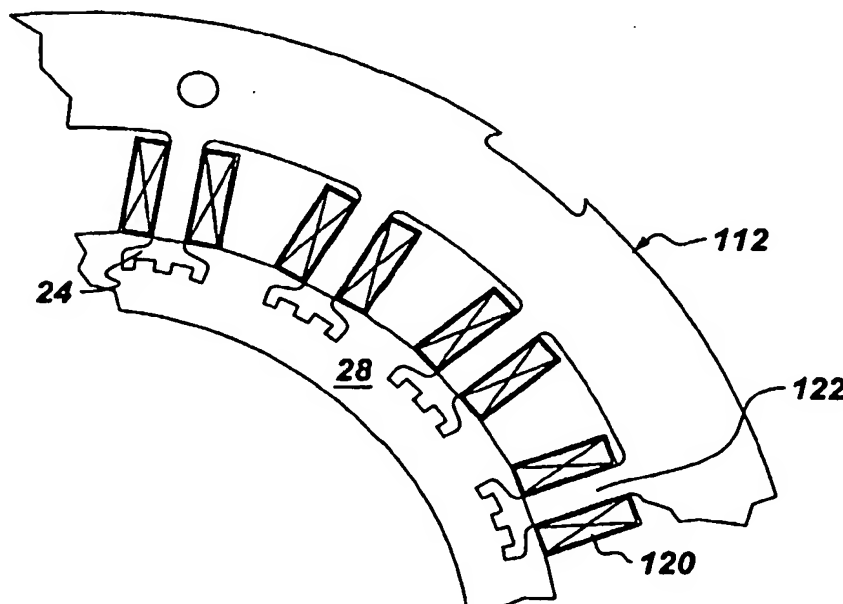
(84) Designated States (*regional*): ARIPO patent (GH, GM, KE, LS, MW, MZ, SD, SL, SZ, TZ, UG, ZM, ZW), Eurasian patent (AM, AZ, BY, EG, KZ, MD, RU, TJ, TM), European patent (AT, BE, BG, CH, CY, CZ, DE, DK, EE, ES, FI, FR, GB, GR, HU, IE, IT, LU, MC, NL, PT, SE, SI, SK, TR), OAPI patent (BF, BJ, CF, CG, CI, CM, GA, GN, GQ, GW, ML, MR, NE, SN, TD, TG).

Published:

— without international search report and to be republished upon receipt of that report

[Continued on next page]

(54) Title: MACHINE STATOR AND FABRICATION METHOD



(57) Abstract: A machine stator (110, 210, 310) is fabricated by positioning pre-wound stator windings (120, 220, 320) with respect to a laminated stator yoke (112, 212) and directly molding composite tooth tips (24) into contact with respective teeth of the laminated stator yoke, or by positioning pre-wound stator windings (21) around respective stator teeth (618) and then coupling the stator teeth and a stator yoke (612), wherein the stator yoke radially surrounds the stator teeth.

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IAP12 Rec'd PCT/PTO 16 JUN 2006

MACHINE STATOR AND FABRICATION METHOD

BACKGROUND

The invention relates generally to electrical machines and more particularly to machine stators.

In the motor industry, it is commercially advantageous to have a motor be as small and cost-efficient as feasible. Conventional motor stators are fabricated by punching laminations with each having an outside diameter and semi-closed slots for insertion of stator windings. The laminations are stacked, annealed, and positioned in an automatic winding machine. Because of the small openings of the slots, the windings cannot be wound in a compact manner and typically occupy no more than about thirty-five percent of the slot area. Thus size reductions of conventional laminated motor stators are limited.

Commonly assigned Kliman et al., US Patent Nos. 5,680,692 and 5,793,138, describe winding insulated coils and then molding a magnetic-flux-carrying stator or rotor around the pre-wound coils. In molded embodiments, the core cannot be annealed to the same extent as a laminated yoke can be annealed due to limitations of the material and of the winding insulation. Thus, depending upon the size of the stator, the molding process has the potential to leave high stresses in the core. Additionally, magnetic powder is significantly more expensive than magnetic laminations.

Commonly assigned Kliman et al., US Patent No. 5,990,588, describes a plurality of circumferentially spaced ferromagnetic strips of various alternative shapes integrally formed in plastic material of a pump assembly enclosure for sealing the stator from fluid in the gap between the stator and rotor. The ferromagnetic strips are described as being in direct contact with respective pole teeth of the stator in a manner which did not noticeably degrade motor performance as compared with fully laminated stator embodiments. Windings are not shown or described.

Commonly assigned Erdman et al., European Patent No. 613,234 B1, describes winding coils (preferably of rectangular cross section) on a conventional high speed bobbin coil winding machine and inserting the wound coils on teeth without tips. In one embodiment of Erdman et al., laminated pole tips can be individually attached to each pole. Erdman et al. describes the individual attachment process as being time-consuming and expensive and provides an alternative embodiment wherein an annulus of alternating interlocking sections of molded extruded powdered iron/plastic composite and non-magnetic plastic sections is slipped into place and located with suitable keys using conventional positioning techniques. In several more specific embodiments of Erdman et al., the coils are wound to conform to the shape of the annulus and the coils are wound into trapezoidal shapes to maximize the use of the space between the stator teeth.

It would be desirable to have a motor fabrication process which more effectively balances the competing goals of low-cost and high-performance.

BRIEF DESCRIPTION

Briefly, in accordance with one embodiment of the present invention, a method for fabricating a machine stator comprises: positioning pre-wound stator windings around respective teeth of a laminated stator yoke; and directly molding composite tooth tips into contact with respective teeth.

In accordance with another embodiment of the present invention, a method for fabricating a machine stator comprises: positioning pre-wound stator windings around respective stator teeth; and then coupling the stator teeth and a stator yoke, wherein the stator yoke radially surrounds the stator teeth.

In accordance with another embodiment of the present invention, a method for fabricating a machine stator comprises: filling end portions of stator windings with non-conducting, non-magnetic particles; and then compacting the end portions.

DRAWINGS

These and other features, aspects, and advantages of the present invention will become better understood when the following detailed description is read with reference to the accompanying drawings in which like characters represent like parts throughout the drawings, wherein:

FIG. 1 is a sectional view illustrating a conventional stator.

FIGs. 2-4 are sectional views illustrating fabrication stages for a stator in accordance with one embodiment of the present invention.

FIGs. 5-8 are sectional views illustrating fabrication stages for a stator in accordance with another embodiment of the present invention.

FIGs. 9-11 are sectional views illustrating fabrication stages for a stator in accordance with another embodiment of the present invention.

FIGs. 12-13 are sectional views illustrating fabrication stages for a stator in accordance with another embodiment of the present invention.

FIG. 14 is a sectional side view illustrating another stator embodiment of the present invention.

DESCRIPTION

FIG. 1 is a sectional view illustrating a conventional stator comprising a stator yoke 12 which in turn comprises stator laminations 14 defining slots 16 and teeth 18. The stator yoke is wound with stator windings 20.

FIGs. 2-11 are sectional views illustrating fabrication stages for a machine stator in accordance with several embodiments of the present invention comprising: (a) positioning pre-wound stator windings 120, 220, 320 around respective teeth 22, 122, 222 of a laminated stator yoke 112, 212; and (b) directly molding composite tooth tips 24 into contact with respective teeth. As used herein "directly molding" means that the act of molding of the tooth tips results in contact with the respective teeth when

molding is complete. Directly molding is in contrast to molding the tooth tips in advance and then inserting the tooth tips into contact with the respect teeth.

The embodiments of FIGs. 2-11 are useful because the stator windings are wound prior to placement around the respective teeth, because a minimal amount of composite material is required, and because the laminated stator yoke (without windings and tooth tips) can be annealed to improve the stator performance.

Referring more specifically to **FIG. 2**, a plurality of compact pre-wound stator windings 120 are positioned around teeth 22. As shown in FIGs. 5-8, key notches can be present in the respective teeth. Windings 120 are typically wound around rectangular bobbins, for example, and radially slid over respective teeth 22. An alternative embodiment includes an automated apparatus 26 (such as an expanding mandrel) on which the wound bobbins are loaded and nested together so that the outer diameter of the bobbin/ winding combination is less than the inner diameter of the stator teeth. The apparatus is then expanded thus sliding all of the bobbins over all of the stator teeth simultaneously.

Laminated stator yoke 112 typically comprises a stack of stator laminations without conventional tooth tips. Laminations of the laminated stator yoke comprise magnetic lamination material such as iron or steel, for example. Windings 120 typically comprise conventional winding material such as copper coated by an insulator such as an enamel, for example. Typically, conventional enamels are suitable for use in any of the embodiments of the present invention because, particularly if the windings are neatly wound in a regular manner without crossovers, conventional enamels are expected to be strong enough to withstand the compression discussed with respect to FIGs. 9-12.

Insulation 144 is typically situated around at least portions of the windings. In one embodiment, the insulation comprises a conventional slot liner type material such as a MYLARTM polyester film or a NOMEXTM synthetic aromatic polyamide polymer film (MYLAR and NOMEX are trademarks of DuPont Co.), for example.

FIG. 3 is a view similar to that of FIG. 2 with the addition of a mold form 28 and composite tooth tip 24 material. The composite tooth tip material typically comprises magnetically conductive particles and a suitable binder. In one embodiment, the composite tooth tip material comprises particles of magnetic material such as iron coated with a polymer, for example. Composite tooth tip material is introduced into mold form 28 by any suitable technique with one example being injection. For some binding materials, curing is useful.

FIG. 4 illustrates the stator 110 after the removal of mold form 28 (Fig. 3). In one embodiment, once the mold form is in place, the composite tooth tip material is filled in from one end, compacting pressure is applied from the filling end, and the mold form is then removed axially. To facilitate removal of the mold form, a conventional mold release compound can be coated on the mold form prior to positioning the mold form. An alternative or additional technique to facilitate removal of the mold form is to incorporate "draft" into the mold. In the draft technique, a small taper is formed from one end of the mold form to the other so that, when the mold is moved, space opens up between the mold form and the molded part.

FIGs. 5-8 are sectional views illustrating fabrication stages for a stator 210 in accordance with another embodiment of the present invention. The embodiment of FIGs. 5-8 is similar to that of the embodiment of FIGs. 2-4 with one difference being that the same volume of pre-wound stator windings can be fit into smaller slots between teeth 222.

FIG. 5 is a sectional view illustrating a mandrel 126 supporting windings 220. In this embodiment, the pre-wound windings 220, wrapped in insulation 244, are longer than teeth 222 (FIG. 6). Mandrel 126 typically comprises fixed parts 129 that bear against the stator teeth forming slots for the long, pre-wound coils. Movable parts 127 push the coils into the slots and compact them radially such that they are contained completely within the slot. The driver for the movable parts is typically mechanical, hydraulic or electromagnetic, for example.

For embodiments wherein compression of wound wires will occur, insulation 244 may beneficially comprise a corrugated material that can be compressed along with the windings.

FIG. 6 is a view similar to that of **FIG. 5** illustrating windings 220 after the windings have been positioned and compressed around respective teeth 222 of laminated stator yoke 212. Teeth 222 of stator yoke 212 are shown as including respective key notches 42 for purposes of illustration. Although it would be feasible to first compress the windings and then position them around the respective teeth, in practice it is expected to be more effective to simultaneously position and compress the windings in place.

FIG. 7 is a view similar to that of **FIG. 6** with the addition of a mold form 128 and composite tooth tip 24 material, and **FIG. 8** illustrates the stator 210 after the removal of the mold form 28. Mold form 128 may comprise a different element from mandrel 126 or mold form 128 may additionally serve as the winding positioning mandrel without the need for a separate element 126.

FIGs. 9-11 are sectional views illustrating fabrication stages (positioning of windings 320 (**FIG. 9**); molding tooth tips 24 (**FIG. 10**); and completed machine stator 310 (**FIG. 11**)) for a stator in accordance with another embodiment of the present invention. The embodiment of **FIGs. 9-11** is similar to the embodiment of **FIGs. 5-8** except that the shape of the stator windings is selected to facilitate fabrication a desired tooth tip 24 shape during molding.

In the embodiments of **FIGs. 9-11**, it is beneficial to compress the windings around respective teeth either prior to or substantially simultaneously with molding of tooth tips 24. "Substantially simultaneously" means that either all winding compression occurs with the compression of composite tooth tip material or some winding compression occurs in advance of the composite tooth tip material compression and some winding compression occurs along with composite tooth tip material compression. Although not shown in **FIGs. 9-11**, insulation of the type described with respect to **FIGs. 2-8** can be used. Similarly, a hollow mandrel, mold form 228, or

combination thereof can be used for positioning, compression, or a combination thereof. The embodiment of FIGs. 9-11 is particularly convenient because the mold form does not need to extend behind the tooth tips and coated magnetic particles can easily be positioned between the mandrel and respective teeth and windings and compressed in the space between the mandrel and the laminated stator yoke.

In one example of compression molding, a driver coil (not shown) is inserted into a mold form and pulsed so as to push the mandrel outward towards the laminated stator yoke. Alternatively, a conventional hydraulic press is used, for example. Regardless of the type of compression that is selected, it is useful to position end caps (not shown) at both ends of the mold to minimize escape of composite tooth tip material.

FIGs. 12-13 are sectional views illustrating fabrication stages for a stator in accordance with another embodiment of the present invention. A method embodiment for fabricating a machine stator 610 comprises: positioning pre-wound stator windings 21 around respective stator teeth 618; and then coupling the stator teeth and a stator yoke 612, wherein the stator yoke radially surrounds the stator teeth.

In a more specific embodiment, the pre-wound stator windings are provided by winding each stator winding to have a wider winding portion 23 and a narrower winding portion 123. The windings can then be positioned around the stator teeth in a manner such that the narrower winding portions are closer to tooth tips 650 than the wider winding portions (and the wider winding portions are closer to the stator yoke). Slots between stator teeth are generally narrower in the tooth tip region than in the stator yoke region, so this embodiment is useful for facilitating sliding of windings 21 and 121 onto stator teeth 618.

In an even more specific embodiment, as shown in FIG. 12, the pre-wound stator windings are provided by flat winding the pre-wound stator windings on a mandrel 626. By using flat (rectangular) coil material, a dense winding and thus a high slot filling ratio (ratio of space filled by stator windings vs. total space) is more readily

achievable. In one embodiment, the stator winding material comprises copper, for example.

As further shown in FIGs. 12-13, a first winding 21 can be wound around a bobbin 626 and then slid over a respective tooth 618. A second winding 121 can likewise be wound around a bobbin and slid over a respective tooth such that portions of windings 21 and 121 are situated in a common slot 616.

The stator teeth comprise any structurally and electromagnetically appropriate material. In one embodiment, the stator teeth comprise laminated stator teeth and a material such as iron, for example. In another embodiment, the stator teeth comprise composite stator teeth and a material such as plastic coated iron particles, for example. In still another embodiment, the stator teeth comprise a combination of laminated and composite materials. In one aspect of the combination embodiment, the stator teeth comprise discrete teeth (typically laminated) and tooth connectors 617 (typically composite) are provided between the stator teeth. Alternatively, the stator teeth may collectively comprise an integral tooth body 619.

Stator yoke 612 comprises any structurally and electromagnetically appropriate material. In one embodiment, stator yoke 612 comprises a laminated stator yoke and a material such as iron, for example. In another embodiment, stator yoke 612 comprises a composite stator yoke and a material such as plastic coated iron particles, for example.

To reduce core losses, in several embodiments stator teeth 618 comprise material having a radially oriented grain, and stator yoke 612 comprises material having an azimuthally oriented grain. In an even more specific related embodiment, stator yoke 612 comprises a laminated stator yoke having an azimuthally oriented grain, and stator teeth 618 comprise composite stator teeth having a radially oriented grain.

In one embodiment, coupling stator teeth 618 and stator yoke 612 comprises shrink-fitting the stator yoke and the stator teeth. Shrink-fitting is typically accomplished by

heating stator yoke 612, dropping stator yoke 612 around stator teeth 618 and windings 21, 121, and allowing stator yoke 612 to cool.

Previously described embodiments of the present invention have many advantages, including effective balance of the competing goals of low-cost and size (from the composite material) and high-performance (from the laminations).

FIG. 14 is a sectional side view illustrating another stator embodiment of the present invention directed to end winding compression by filling end portions 40 of stator windings with non-conducting, non-magnetic particles 38, and compacting the end portions and the particles. The embodiment of FIG. 14 is useful both in electronically commutated machines and induction machines, for example, whether the stator is entirely laminated, entirely molded, or a combination of laminations and molding.

To minimize the extent of particles 38 within the stator yoke, dividers 36 can be used between the stator yoke and the end winding regions. In one embodiment, the dividers comprise thin plastic membranes, for example, which are later either removed or left in place.

For the compression, the end winding region is typically surrounded by mandrel 30, outer mold form 32, and end plates 34, for example, each of which comprises a material with sufficient structural integrity to withstand the compression process. One embodiment uses steel, for example. The compression itself is directed from any of the three directions (mandrel 30, mold form 32, or end plates 34) or a combination of the three directions.

After the end windings are compacted, non-magnetic particles 38 may optionally be removed. Alternatively, particularly if filling the end portions comprises filling the end portions with material comprising the non-conducting non-magnetic particles and a binder, the material may conveniently be left in place after compaction. Leaving the material in place can beneficially result in the stator being resistant to moisture, having improved heat transfer properties, and having increased mechanical stability.

Managing the end windings space has several advantages in that end windings may physically limit the amount of compression that can be used for regular windings and teeth, and added inductance from regularly designed end windings can be detrimental to electrical controls of the machine.

While only certain features of the invention have been illustrated and described herein, many modifications and changes will occur to those skilled in the art. It is, therefore, to be understood that the appended claims are intended to cover all such modifications and changes as fall within the true spirit of the invention.

CLAIMS:

1. A method for fabricating a machine stator (110) comprising:
 - (a) positioning pre-wound stator windings (120) around respective teeth (18) of a laminated stator yoke (112); and
 - (b) directly molding composite tooth tips (24) into contact with respective teeth of the laminated stator yoke.
2. The method of claim 1 wherein positioning comprises compressing the pre-wound stator windings around the respective teeth.
3. A machine stator (310) comprising:
 - (a) stator windings (320) comprising a wound shape designed to provide space for a desired tooth tip shape;
 - (b) a laminated stator yoke (212) situated around the stator windings; and
 - (c) molded composite tooth tips (50) between respective windings and in contact with the laminated stator yoke.
4. The machine stator of claim 3 further comprising, insulation around at least portions of the stator windings.
5. The machine stator of claim 4 wherein the insulation comprises corrugated material.
6. A method for fabricating a machine stator (510) comprising:
 - (a) filling end portions (40) of stator windings with non-conducting, non-magnetic particles (38); and then
 - (b) compacting the end portions.
7. A method for fabricating a machine stator (110) comprising:

(a) positioning pre-wound stator windings (21) around respective stator teeth (618); and then

(b) coupling the stator teeth and a stator yoke (612), wherein the stator yoke radially surrounds the stator teeth.

8. A machine stator (110) comprising:

(a) stator windings (21) around respective stator teeth (618); and

(b) a stator yoke (612) radially surrounding and coupled to the stator teeth.

9. The stator of claim 8 wherein each stator winding comprises a wider winding portion (23) and a narrower winding portion (123) with the wider winding portion situated closer to the stator yoke than the narrower winding portion.

10. The stator of claim 8 wherein the stator teeth comprise material having a radially oriented grain, and wherein the stator yoke comprises material having an azimuthally oriented grain.

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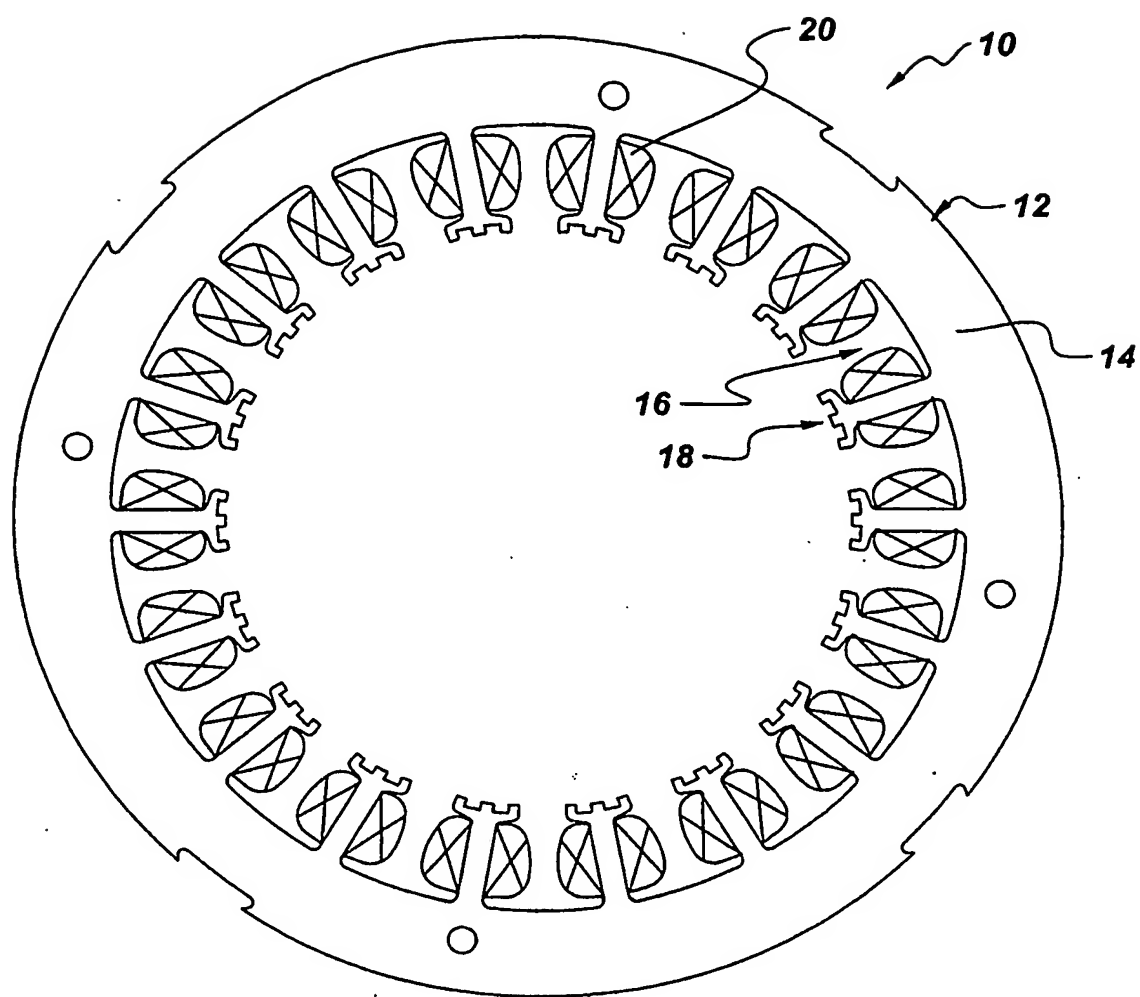
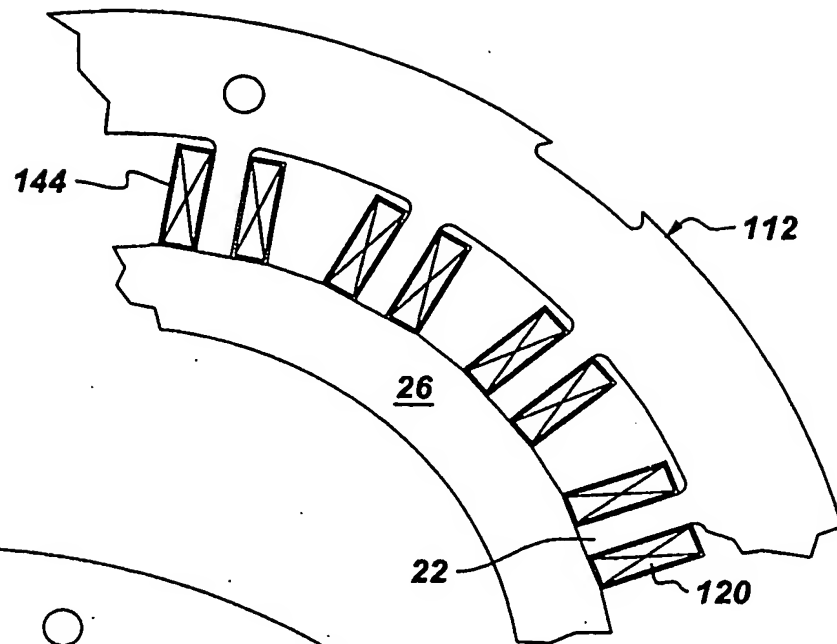
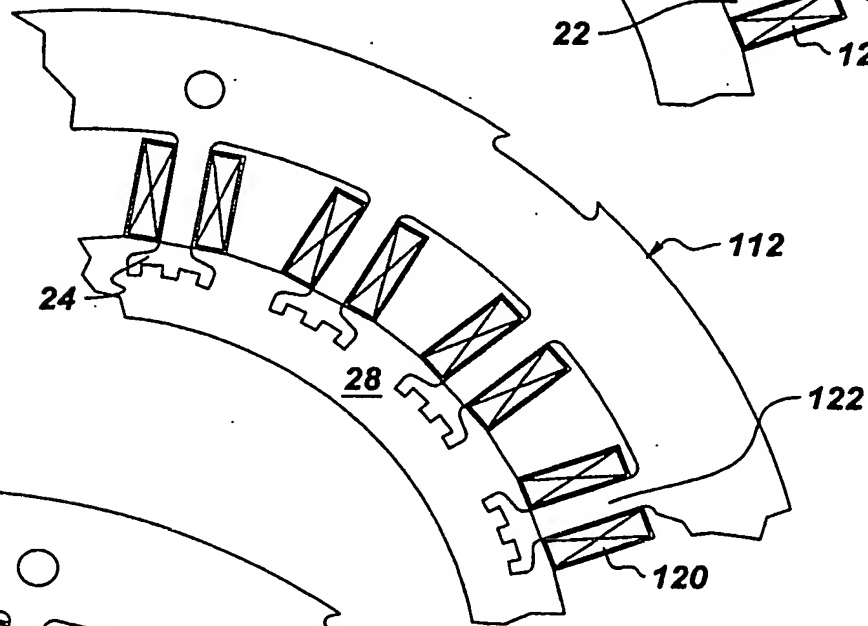
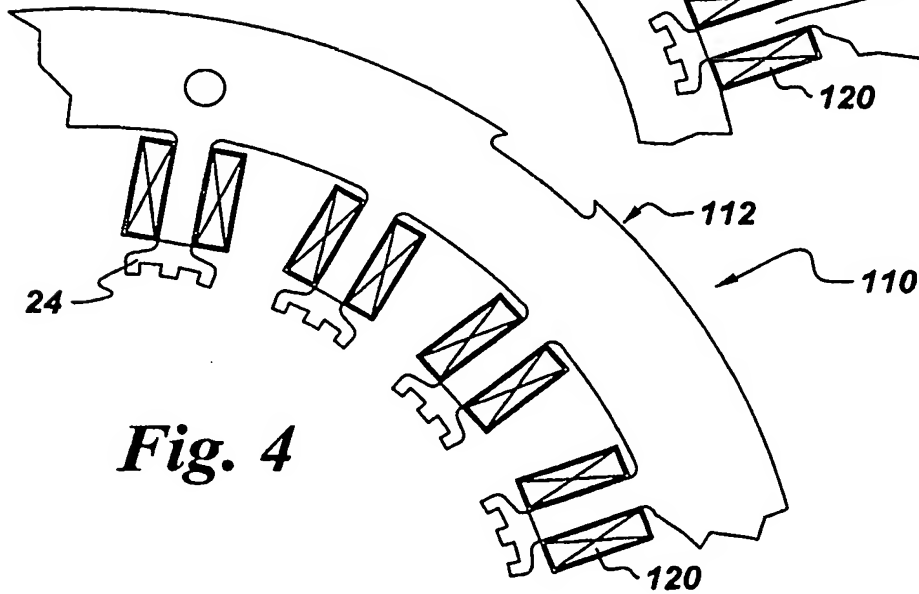


Fig. 1
(Prior Art)

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Fig. 2**Fig. 3****Fig. 4**

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Fig. 5

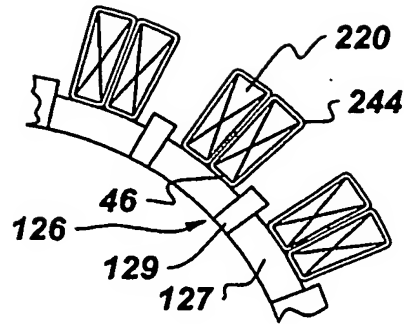


Fig. 6

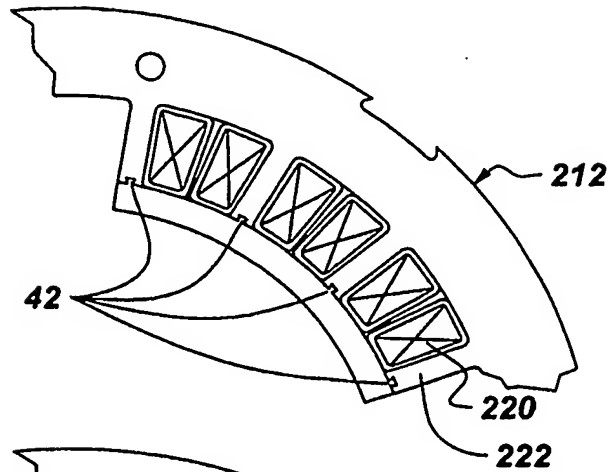


Fig. 7

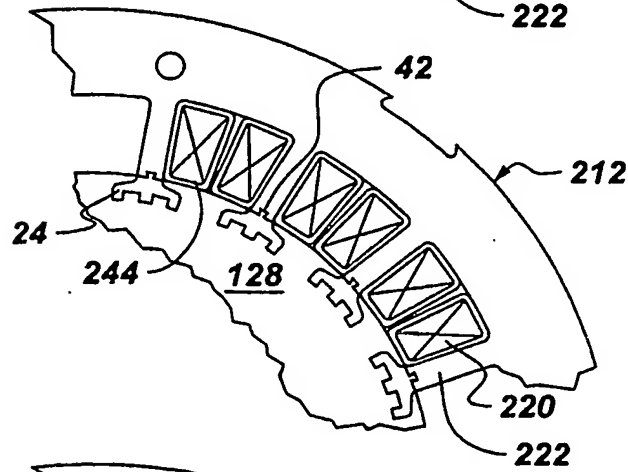
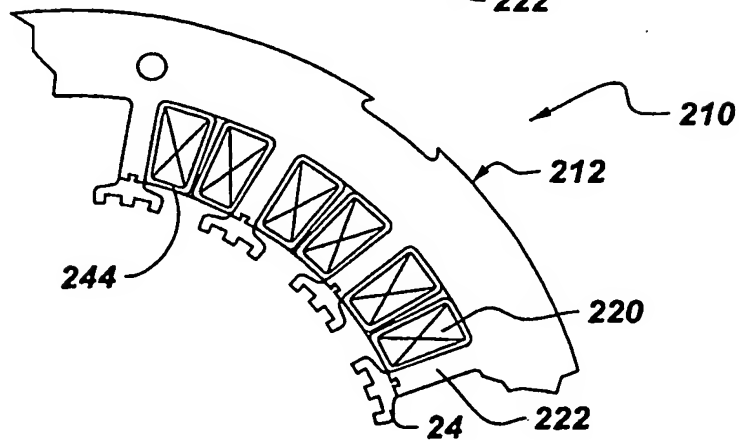
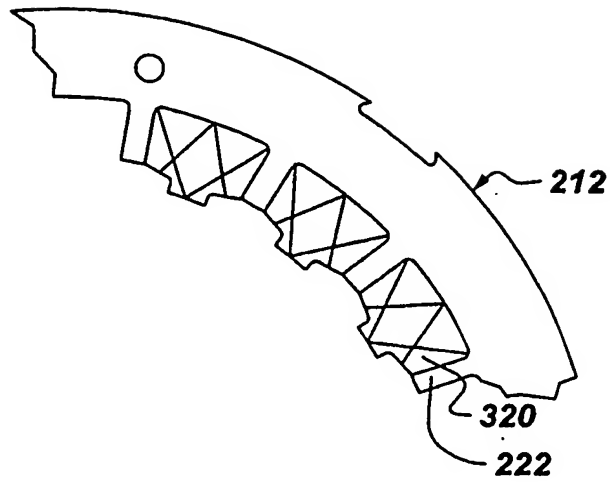
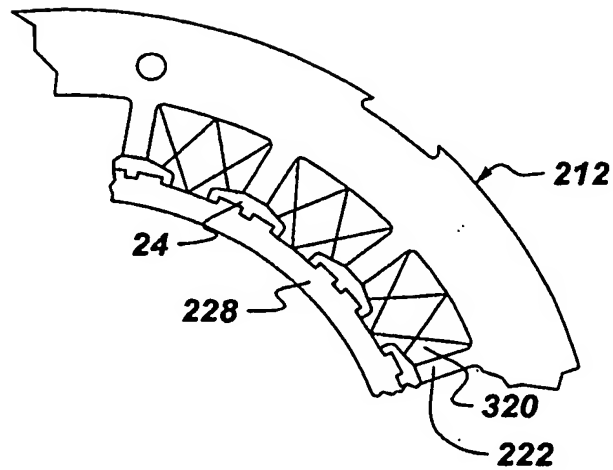
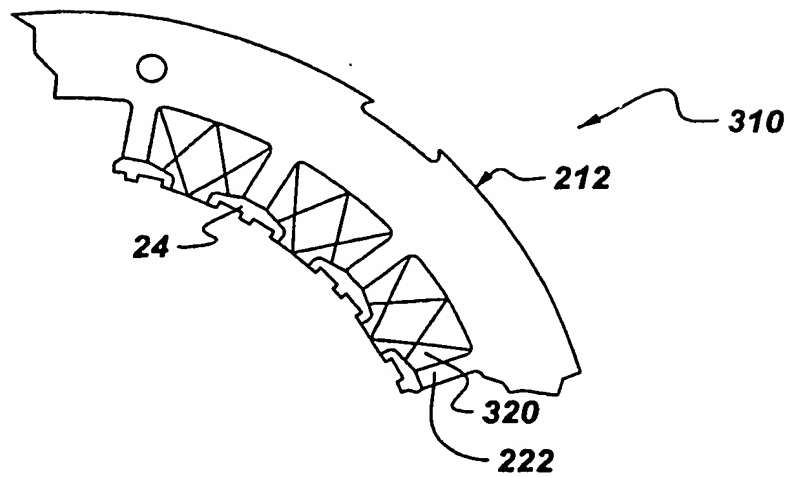


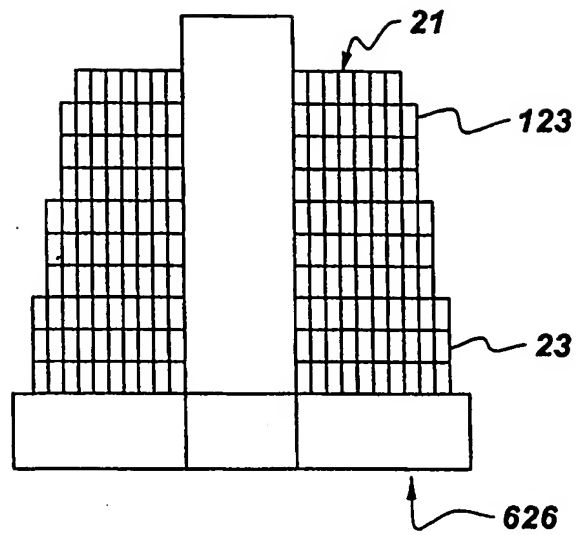
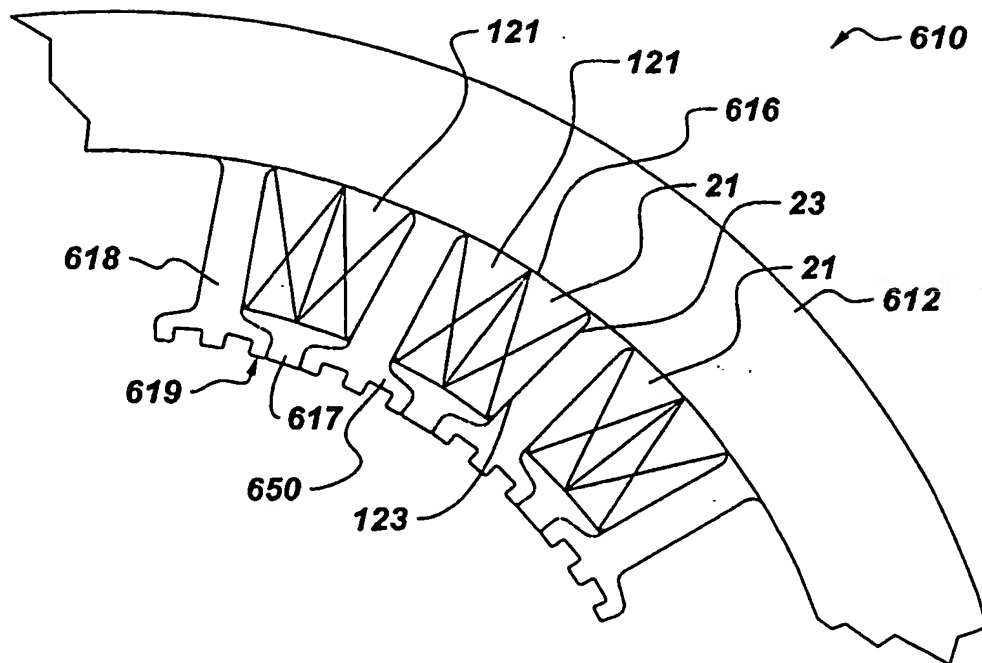
Fig. 8



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Fig. 9**Fig. 10****Fig. 11**

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**Fig. 12****Fig. 13**

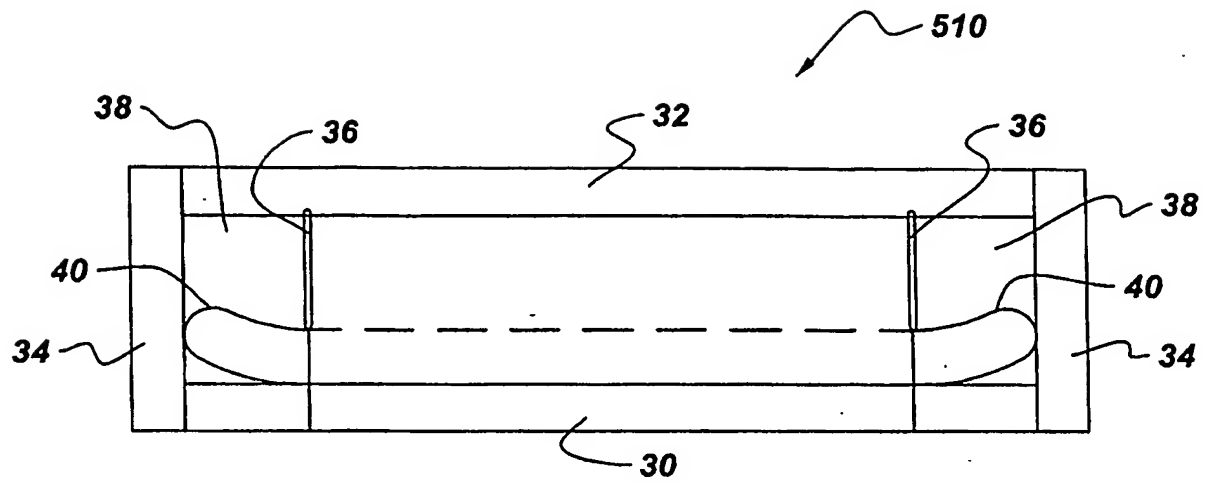


Fig. 14

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